

CALCULATIONS



Project A96 Threapland										
JEN	S100630					Date 17/12/07	Page No 1 of 4			Rev ↙
Originator NAW		Checked MCH 18/12/07		Revision	Suffix	Orig				
					Date	Check				
Ref. DMRB HA 216/06 Annex 1	<p style="text-align: center;"><u>WATER RESOURCES CHAPTER - DMRB</u> <u>WATER QUALITY CALCULATIONS</u></p> <p style="text-align: center;"><u>METHOD A</u></p> <p>$V_R \Rightarrow Q_{95} = 40 \text{ m}^3/\text{d}$ (see low flow calculation attached)</p> <p>AA DT (Two-way) = Existing traffic flow * NRTF Growth Factor</p> <p style="margin-left: 40px;">= 15,000 * 1.292</p> <p style="margin-left: 40px;">= <u>19,380</u></p> <p>$V_H \Rightarrow$ Rainfall = 13mm/day (Figure A.1)</p> <p style="margin-left: 40px;">Run off coefficient = 0.5</p> <p style="margin-left: 40px;">Road area = 1200 * 7.5 m</p> <p style="margin-left: 80px;">Length Carriageway width</p> <p>$V_H = 0.5 * (13 \div 1000) * (1200 * 7.5)$</p> <p style="margin-left: 40px;">= <u>58.5 m³</u></p> <p>Based on $V_R/V_H = \frac{40}{58.5} = 0.68$ &</p> <p>Figure A.2 this immediately puts the watercourse at high risk, and therefore a detailed assessment is required.</p> <p style="text-align: center;"><u>METHOD B</u></p> <p style="text-align: center;"><u>Copper</u></p> <p>$CR = \left[\left[(C_B * V_R) + (1000 * M) \right] / (V_R + V_H) \right]$</p> <p>$C_B =$ u/s dissolved Copper = 4 µg/L</p> <p>$V_R = 40 \text{ m}^3/\text{d}$</p> <p>$M = 0.4 * \frac{5}{365} * \left(\frac{1200 * 7.5}{10,000} \right)$</p> <p>Table B.1</p> <p>$M = 0.005 \text{ kg}$</p>								Output	
Chapter 2 ES										
Refer to Water Quality Sampling Results Attached										

CALCULATIONS



Project A96 Threapland									
JEN S100630			Date 17/12/07			Page No 2 of 4			Rev ↓
Originator NAW		Checked MCH 18/12/07		Revision	Suffix	Orig			
		Date	Check						
Ref.	<p>CR = $\frac{[(4 \times 10^{-3} \times 40) + (1000 \times 0.065)]}{(40 + 58.5)}$</p> <p>CR = 0.052 kg/m³</p> <p>CR = 52 µg/l</p> <p>Table 2.1 DMRB "A2" = RE2 Compare this to the EQS for an RE2 watercourse (i.e. assumed water quality of the Loch Oire Outfall Drain) of <u>40 µg/L</u> (for hardness of < 100mg/L)</p> <p>See Water Quality Sample Results Note - hardness was measured as 100 mg/L.</p> <p>Therefore, this will result in a slight exceedance of the EQS.</p> <p><u>ZINC</u></p> <p>CR = $[(C_B \times V_R) + (1000 \times M)] / (V_R + V_H)$</p> <p>C_B = u/s dissolved zinc = 23 µg/L</p> <p>V_R = 40m³/d</p> <p>M = 2.0 × 5/365 × $(\frac{1200 \times 7.5}{10,000})$</p> <p>Table B.1</p> <p>M = 0.025 kg</p> <p>CR = $\frac{[(23 \times 10^{-3} \times 40) + (1000 \times 0.025)]}{(40 + 58.5)}$</p> <p>CR = 0.263 kg/m³</p> <p>CR = 263 µg/L</p> <p>Table 2.1 DMRB "A2" = RE2 Compare this to the EQS for an RE2 watercourse (i.e. assumed water quality of the Loch Oire Outfall Drain) of <u>300 µg/L</u> (for hardness of < 100mg/L)</p> <p>See Water Quality Sample Results Note - hardness was measured as = 100mg/L (as above)</p> <p>Therefore, this does not exceed the EQS & is OK.</p>								Output
									>EQS ∴ Some impact.
									<EQS ∴ OK

CALCULATIONS



Project A96 Threapland											
JEN	S1100630			Date	17/12/07			Page No	3 of 4		Rev
Originator		Checked		Revision	Suffix	Orig					
NAW		MCH 18/12/07			Date	Check					
Ref.	<p style="text-align: center;"><u>Method D</u></p> <p>$P_{ACC} = RL * SS * (AADT * 365 * 10^{-9}) * (\% HG V / 100)$ $AADT = 19,380$ $\% HG V = 10\%$ (Ref. email from SW Roads Team (D. Mackenzie) dated 20/08/07)</p> <p>The stretch of the A96 under consideration contains:-</p> <ul style="list-style-type: none"> • Two cross roads • Three side roads <p>In the existing situation, which will become:-</p> <ul style="list-style-type: none"> • One cross road, r • four side roads <p>under the proposed scheme.</p> <p>Table D.1 * Assume A96 is a "rural trunk road".</p> <p><u>Proposed situation</u></p> <p>$P_{ACC} = (4 * 0.3 km) * 0.93 * (19380 * 365 * 10^{-9}) * (10/100)$ $= 7.9 * 10^{-4}$</p> <p>$P_{ACC} = (1 * 0.4 km) * 0.88 * (19380 * 365 * 10^{-9}) * (10/100)$ $= 2.5 * 10^{-4}$</p> <p>$P_{ACC} = (1.4 - 1.0) * 0.29 * (19380 * 365 * 10^{-9}) * (10/100)$ (Trunk Road) Total length Length already accounted for above $= 8.2 * 10^{-5}$</p> <p>$P_{ACC} = 1.12 * 10^{-3}$ (Total)</p> <p>Table D.2 $P_{INC} = P_{ACC} * P_{POL} = 1.12 * 10^{-3} * 0.6$ $= 6.72 * 10^{-4} = 0.067\% \ll 1\%$</p>									Output	
										<u>OK</u>	

CALCULATIONS



Project A96 Threapland											
JEN	S100630				Date	17/12/07		Page No	4 of 4		Rev
Originator	Checked		Revision	Suffix	Orig						
NAW	MCH 18/12/07			Date	Check						
Ref.	<u>Method C</u>									Output	
	Component No.	Property	Weighting Factor	Site Data	Risk Score	Component Score					
	1	Traffic density	15	19,380 for 2028	Medium (2)	30					
	2	Rainfall	15	≈ 806 mm (FEH) 1hr rainfall ≈ 33mm (FEH)	Medium (2)	30					
	3	Soakaway Geometry	15	Filter Drains & Retention Pond	Medium (2)	30					
	4	Unsaturated Zone	20	Depth < 5m under retention pond	High (3)	60					
	5	Flow Type	20	Mixed fracture & inter-granular flow	Medium (2)	40					
	6	Effective Grain Size	7.5	Predominantly coarse sand	Medium (2)	15					
	7	Lithology	7.5	1-5% Clay Minerals (Est. from GI)	Medium (2)	15					
	Therefore, the overall score is between 150 → 250 and the ground-water is at a medium risk of impact. ∴ apply mitigation measures.									<u>220</u>	

Validated
 Preliminary

ALcontrol Geochem Analytical Services Table Of Results

ISO 17025 accredited
 M MCERTS accredited
 * Subcontracted test
 » Shown on prev. report

Job Number: 07/21421/02/01
Client: Norwest Holst Ltd
Client Ref. No.: F14909

Matrix: LIQUID
Location: A96 THREAPLAND
Client Contact: Kenny McLaren

Sample Identity	WS01																				Method Code	Lod/Units		
Depth (m)	-																							
Sample Type	LIQUID																							
Sampled Date	22.11.07																							
Sample Received Date	03.12.07																							
Batch	1																							
Sample Number(s)	1-2																							
Hardness Total	100																					TM152 [#]	<1 mg/l	
Arsenic Dissolved (ICP-MS)	<1																						TM152 [#]	<1 ug/l
Boron Dissolved (ICP-MS)	16																						TM152 [#]	<10 ug/l
Cadmium Dissolved (ICP-MS)	<0.4																						TM152 [#]	<0.4 ug/l
Chromium Dissolved (ICP-MS)	4																						TM152 [#]	<1 ug/l
Copper Dissolved (ICP-MS)	4																						TM152 [#]	<1 ug/l
Iron Dissolved (ICP-MS)	<5																						TM152 [#]	<5 ug/l
Lead Dissolved (ICP-MS)	2																						TM152 [#]	<1 ug/l
Nickel Dissolved (ICP-MS)	<1																						TM152 [#]	<1 ug/l
Selenium Dissolved (ICP-MS)	<1																						TM152 [#]	<1 ug/l
Zinc Dissolved (ICP-MS)	23																						TM152 [#]	<3 ug/l
Mercury Dissolved (CVAF)	<0.01																						TM183 [#]	<0.01 ug/l
Total Alkalinity as CaCO3	100																						TM043 [#]	<2 mg/l
BOD	3																						TM045 [#]	<1 mg/l
COD	22																						TM107 [#]	<5 mg/l
Dissolved Oxygen	9																						TM046	<1 mg/l
Conductivity (at 25 deg.C)	0.26																						TM120 [#]	<0.014 mS/cm
Sulphate (soluble)	6																						TM098 [#]	<3 mg/l
Phosphate (Ortho as PO4)	<0.08																						TM100 [#]	<0.08 mg/l
Sulphide																							TM101	<0.5 mg/l
Ammoniacal Nitrogen as N	0.2																						TM099 [#]	<0.2 mg/l
Hexavalent Chromium																							TM151 [#]	<0.03 mg/l
Phenols Monohydric	<0.01																						TM062 [#]	<0.01 mg/l
Thiocyanate	<0.05																						TM153 [#]	<0.05 mg/l
Total Cyanide	<0.05																						TM153 [#]	<0.05 mg/l
Free Cyanide	<0.05																						TM153 [#]	<0.05 mg/l
Complex Cyanide	<0.05																						TM153 [#]	<0.05 mg/l
pH Value	8.10																						TM133 [#]	<1.00 pH Units

Date 18.12.2007

Scheme: A96 Threapland

Catchment Yield Analysis - Loch Oire Outfall Drain

Description	Value	Comments
Basic Data:		
Catchment Area (km ²)	0.750	1:25,000 OS maps] NOTE FEH RECORDS CATCHMENT @ 2.3km²
Total Loch Area in Catchment (km ²)	0.060	1:25,000 OS maps and bathymetry survey
Loch Area for Supply Loch only (km ²)	0.060	Bathymetry survey
SAAR (mm)	800.00	Average Annual Rainfall Map (Wallingford)
Annual Potential Evapotranspiration (PE), (mm)	400.00	Estimate from previous work
Base Flow Index (BFI)	0.320	Estimate from Scotland BFI Map
Low Flow Duration "D" (days)	0.00	L NOTE FEH RECORDS BFI @ 0.885
Low Flow Return Period "RP" (years)	0.00	
Low Flow Probability	#DIV/0!	
Q95(1) :		
Average Daily Flow (ADF or MF), (m ³ /s)	0.010	
Average Daily Flow (ADF or MF), (m ³ /d)	822	
FLAKE, (Loch Area/Catchment Area)	0.080	
Flow Duration Period, (days)	10.00	IoH Report 101
Flow Duration Curve, (Q95(10)) ^{1/2}	2.35	
Q95(10), (%ADF)	5.51	
log ₁₀ GRADQ95	-1.91	
GradQ95	0.01	
Q95(1), (%ADF)	4.90	Using Low Flow Studies Report 2.1 (1980)
Q95(1) - (m ³ /day)	40	

∴ Q95 estimated is deemed to be conservative