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Job No. and Title	EGIP Strategic Review	Originator	GMcF	Date	12 May 2012
Work Section	Buffer Stop Calculations	Checker		Date	

Minimum mass = 74.7 t (2 car Class 156 as supplied by Transport Scotland)

Maximum mass = 335.16 t (8 car Class 380 as supplied by Transport Scotland)

Assumptions

Calculations are based on buffer stop type 22EB/3

Twin friction element of 3No. Bolt clamps, Torque 150 Nm under buffer stop on running rails

Breaking = 80 kJ/m

3 pairs of twin friction element (3 clamp bolts per element), Torque 150 Nm behind buffer stop

E = 240 kJ/m

Assume track is level - no potential energy considered

For Class 156

Vehicle Data Train mass m = 74.7 t

Max. impact speed v = 10 km/h = 2.78 m/s

Deceleration d = $\leq 1.47 \text{ m/s}^2$ = 0.15 g

Kinetic energy at impact Ekin =
$$\frac{m \times v^2}{2} = \frac{74.7 \times 2.78^2}{2} = 289 \text{ kJ}$$

Energy absorption of buffer stop:

Distance to second stage normally 3.5 m

Breaking capacity = $3.5 \times 80 = 280 \text{ kJ}$

Distance required to arrest Clas 156 = 3.613 m

Therefore, contact with second stage would be minimal.

Check deceleration -
$$d = \frac{v^2}{2 \times s} = \frac{2.78^2}{2 \times 3.613} = 1.07 \text{ m/s}^2$$
 = 0.109 g Therefore, OK

Stopping distance = 3.613 m

Buffer length = 2.4 m

Additional retarders = 0 m

Total track occupancy = 6.013 m

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For Class 380

Vehicle Data Train mass $m = 335.16 \text{ t}$

Max. impact speed $v = 10 \text{ km/h} = 2.78 \text{ m/s}$

Deceleration $d = \leq 1.47 \text{ m/s}^2 = 0.15 \text{ g}$

$$\text{Kinetic energy at impact} \quad E_{\text{kin}} = \frac{m \times v^2}{2} = \frac{335.16 \times 2.78^2}{2} = 1295.125 \text{ kJ}$$

Energy absorption of buffer stop (normal slave spacing):

First stage $3.5 \times 80 \text{ (1 pair)} = 280 \text{ kJ}$

Second stage $0.5 \times 160 \text{ (2 pairs)} = 80 \text{ kJ}$

Third stage $0.5 \times 240 \text{ (3 pairs)} = 120 \text{ kJ}$

Fourth stage $2.6 \times 320 \text{ (4 pairs)} = 832 \text{ kJ}$

$s = 7.1 \text{ m} = 1312 \text{ kJ}$

$$\text{Check deceleration - } d = \frac{v^2}{2 \times s} = \frac{2.78^2}{2 \times 7.1} = 0.544 \text{ m/s}^2 = 0.055 \text{ g} \quad \text{Therefore, OK}$$

Total occupancy for normal slave spacing and normal number of slaves

Stopping distance $= 7.1 \text{ m}$

Buffer length $= 2.4 \text{ m}$

Additional retarders $= 0.75 \text{ m}$

Total track occupancy $= 10.25 \text{ m}$

10.25 m would give Deceleration value of 0.055 g

0.15 g is allowable

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Energy absorbtion of buffer stop (adding 1 No. pair of slaves at each location):

First stage		3.5×80	(1 pair)	=	280 kJ
Second stage		0.5×240	(3 pairs)	=	120 kJ
Third stage		0.5×400	(5 pairs)	=	200 kJ
Fourth stage		1.5×560	(7 pairs)	=	840 kJ

Check deceleration -	$d = \frac{v^2}{2 \times s} = \frac{2.78^2}{2 \times 6}$	= 0.644 m/s ²
		= 0.065 g Therefore, OK

$$\text{Stopping distance} = 6 \text{ m}$$

Buffer length = 2.4 m

Additional retarders = 1.5 m

Total track occupancy = **9.9 m**

Energy absorbtion of buffer stop (adding 2 No. pair of slaves at each location):

First stage		3.5×80	(1 pair)	=	280 kJ
Second stage		0.5×400	(5 pairs)	=	200 kJ
Third stage		0.5×560	(7 pairs)	=	280 kJ
Fourth stage		0.7×880	(11 pairs)	=	616 kJ

Check deceleration -	$d = \frac{v^2}{2 \times s} = \frac{2.78^2}{2 \times 7.1}$	=	0.743 m/s ²	
		=	0.076 g	Therefore, OK

Total occupancy for normal slave spacing and normal number of slaves

$$\text{Stopping distance} = 5.2 \text{ m}$$

Buffer length = 2.4 m

Additional retarders = 2.75 m

Total track occupancy = **10.35 m**